

Motor Driver ICs

Power Dissipation and PCB Layout

Pete Millett

Senior Technical Marketing Engineer

May 2020



Pete Millett – Senior Technical Marketing Engineer



2014–Present

- MPS Senior Technical Marketing Engineer for motor driver ICs
- Responsible for new product definitions as well as application engineering

2005–2013

- Systems Engineer and Systems Manager at Texas Instruments
- Product definition and systems engineering for motor driver ICs (DRV8XXX)

1982–2005

- Board-level hardware design engineer at various computer and consumer electronics companies

Introduction to Motor Driver ICs

Power Dissipation in Drivers

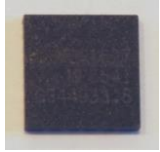
PCB Design for Power Dissipation

Summary / Q&A

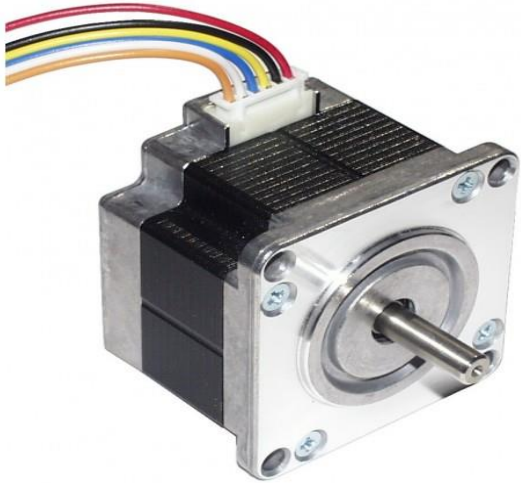
An Introduction to Motor Driver ICs



Brushed DC Motor

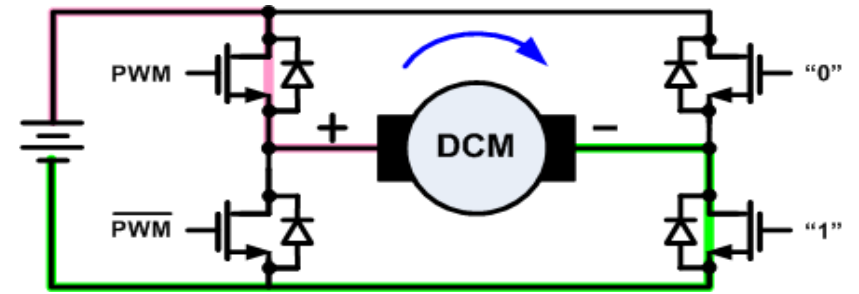
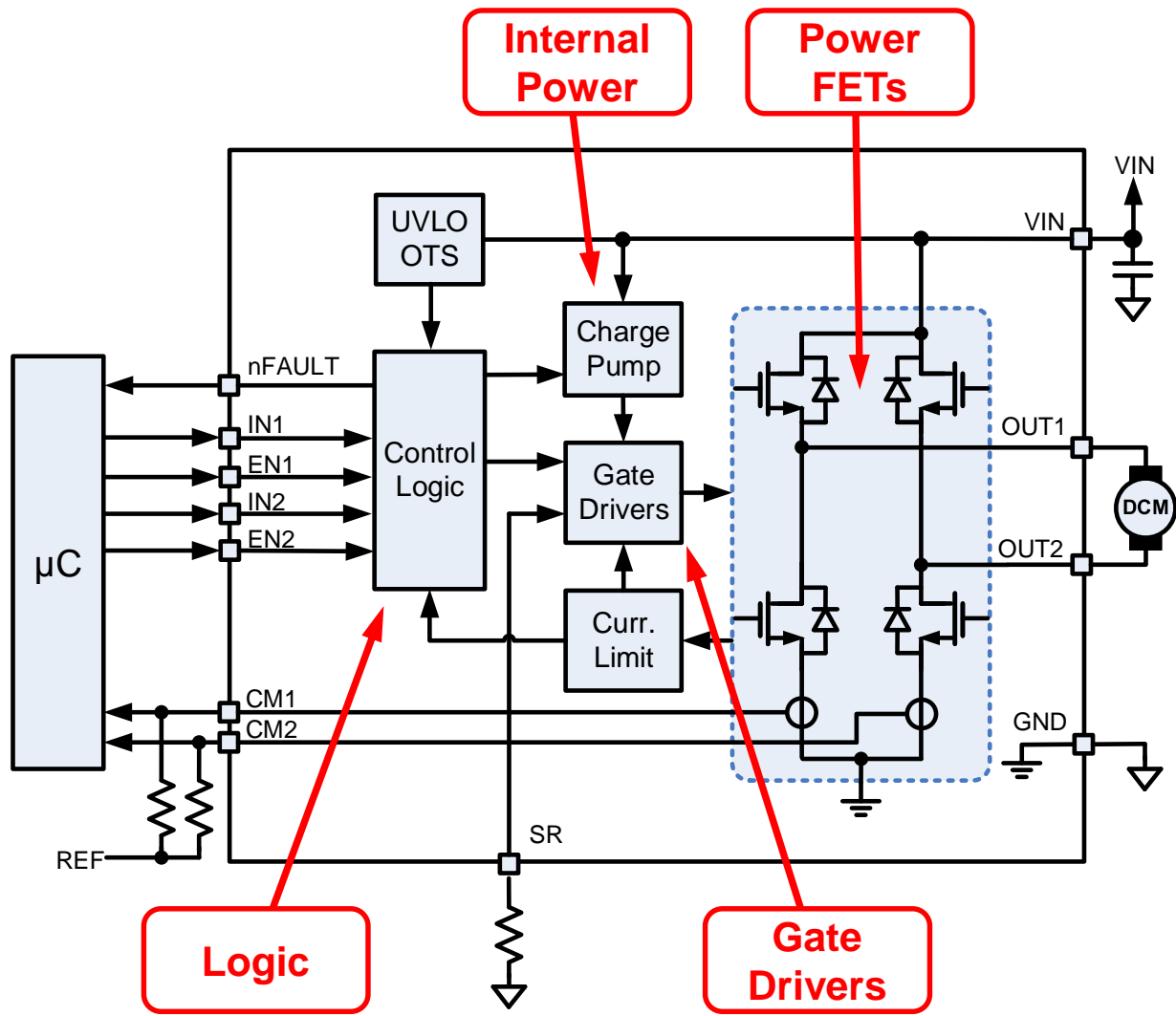


Brushless DC Motor



Stepper Motor

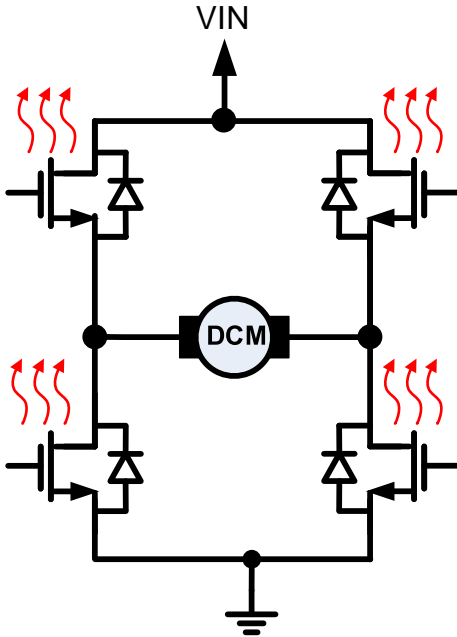
Inside a DC Motor Driver IC



Power Dissipation in Motor Drivers

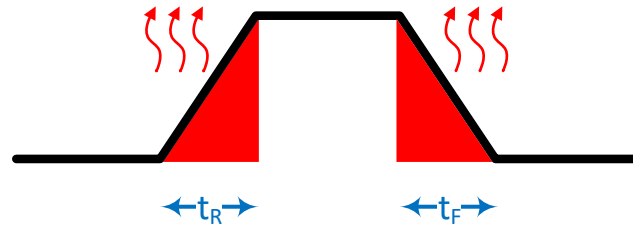
Resistive Losses

$$P_R = I^2 R$$



Switching Losses

$$P_S \approx \frac{1}{2} \times V \times I \times f_{sw} \times t_R + \frac{1}{2} \times V \times I \times f_{sw} \times t_F$$



Static Losses

$$P_Q = V_{IN} \times I_Q$$

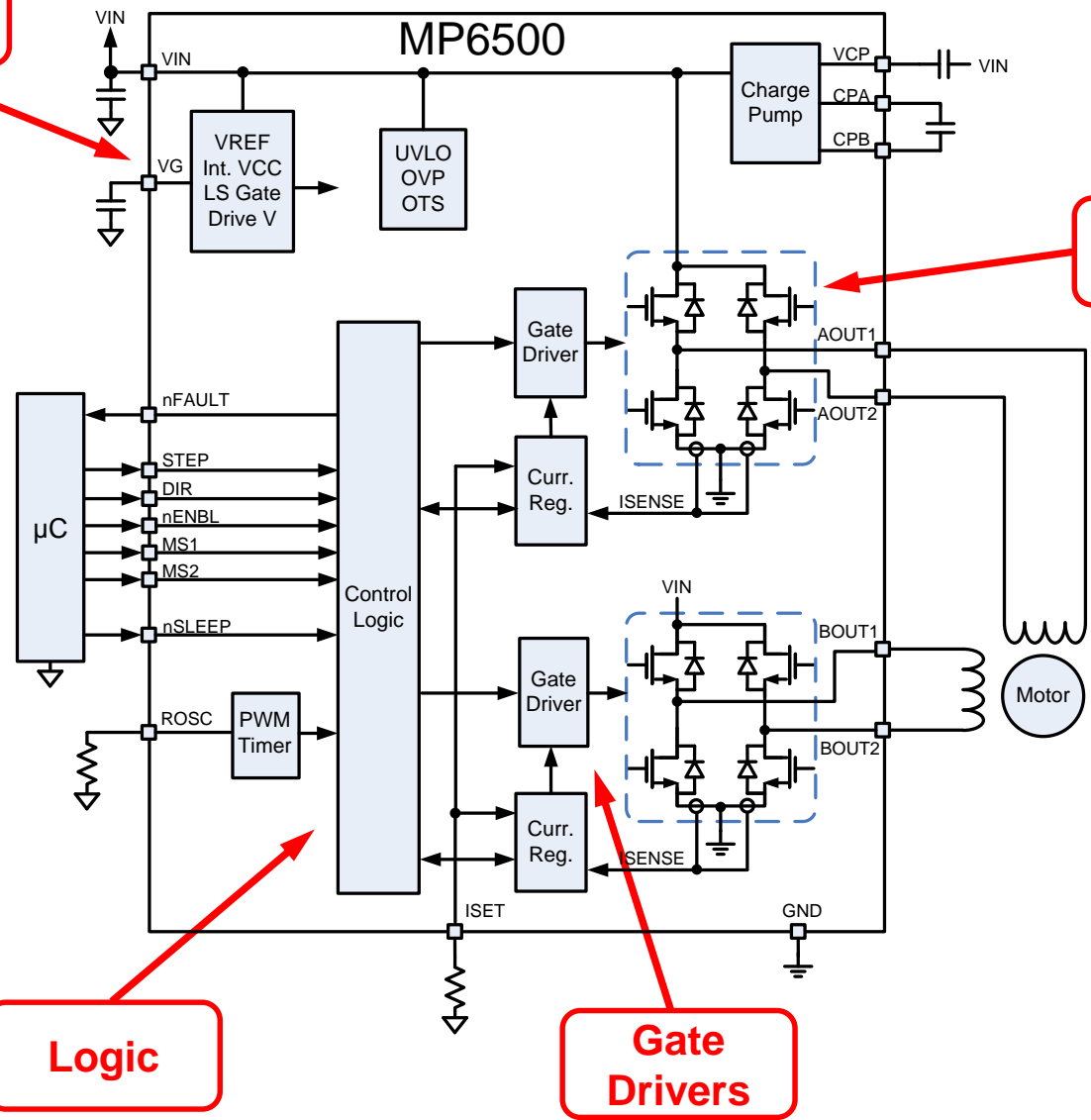


Total Power

$$P = P_R + P_S + P_Q$$

Power Dissipation in Stepper Motor Driver ICs

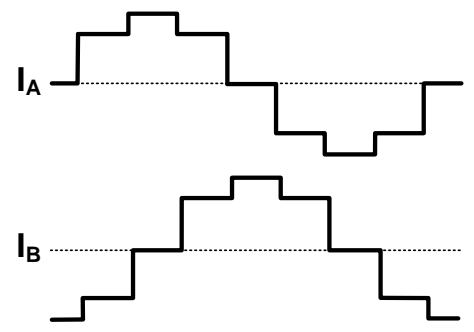
Internal Power



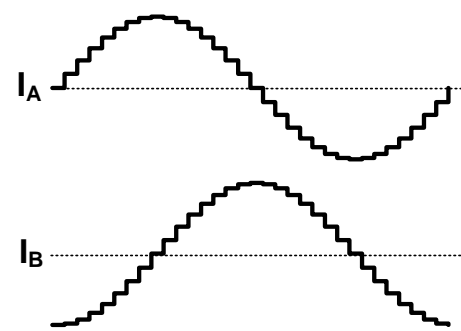
Power FETs

Logic

Gate Drivers

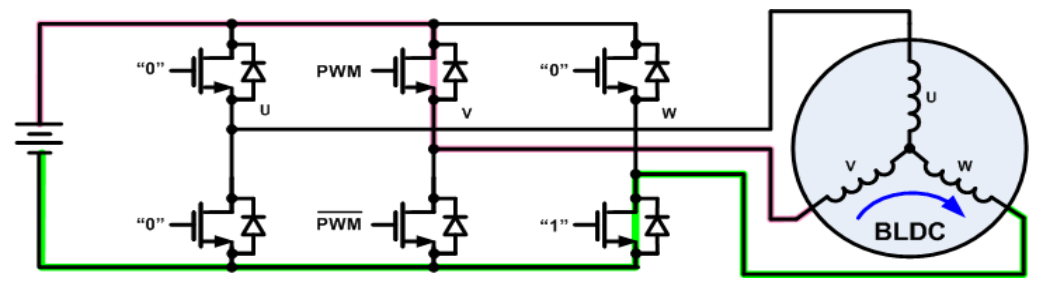
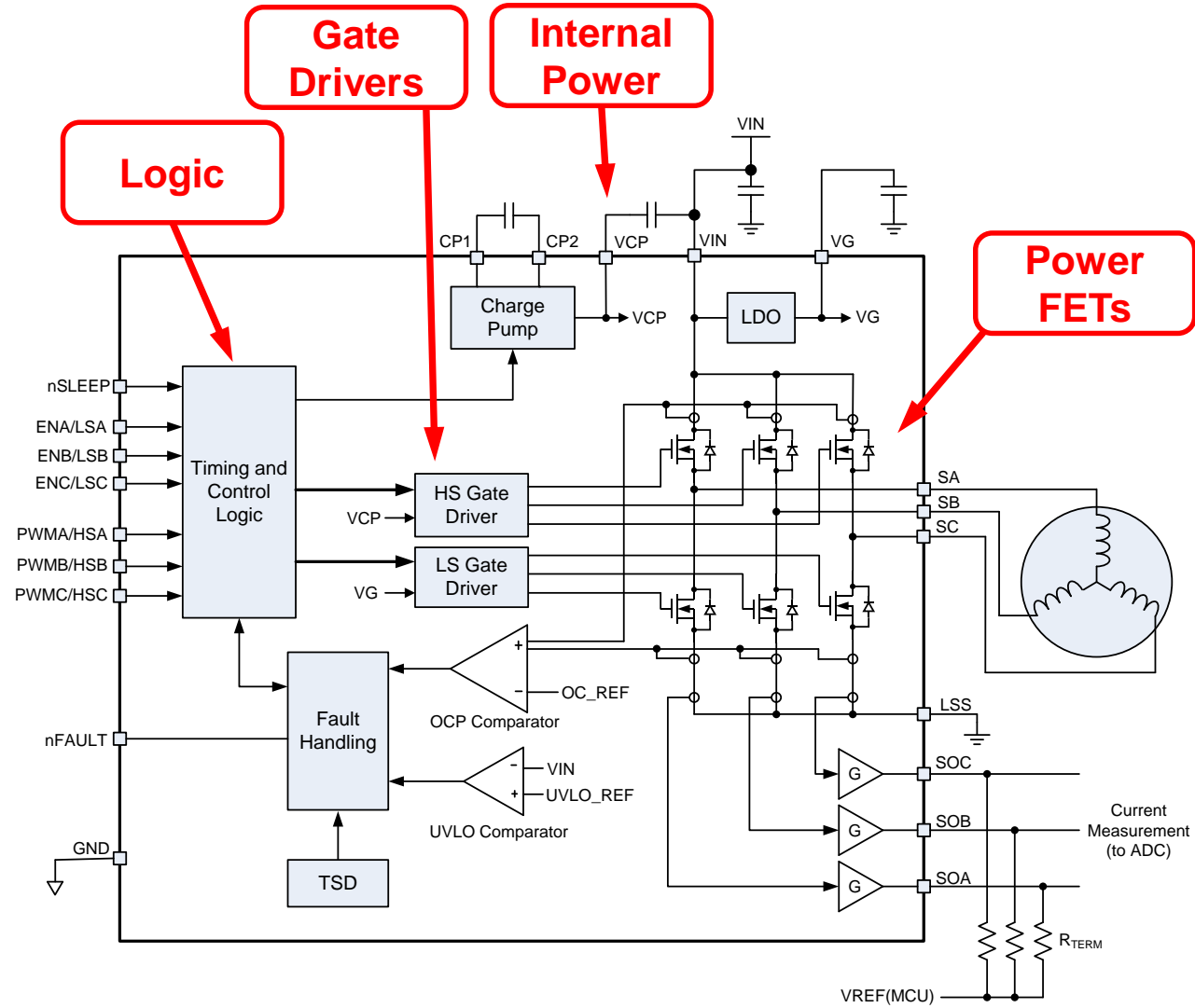


8 Segments Half-Step



32 Segments Eighth-Step

Brushless Motor Drivers



Power Dissipation Example

Using the MP6550 IC as an example:

HS Switch-On Resistance	R _{DS(ON)}	IO=800mA, Ta = 25°C,		0.1	0.13	Ω
LS Switch-On Resistance	R _{DS(ON)}	IO=800mA, Ta = 25°C,		0.1	0.13	Ω

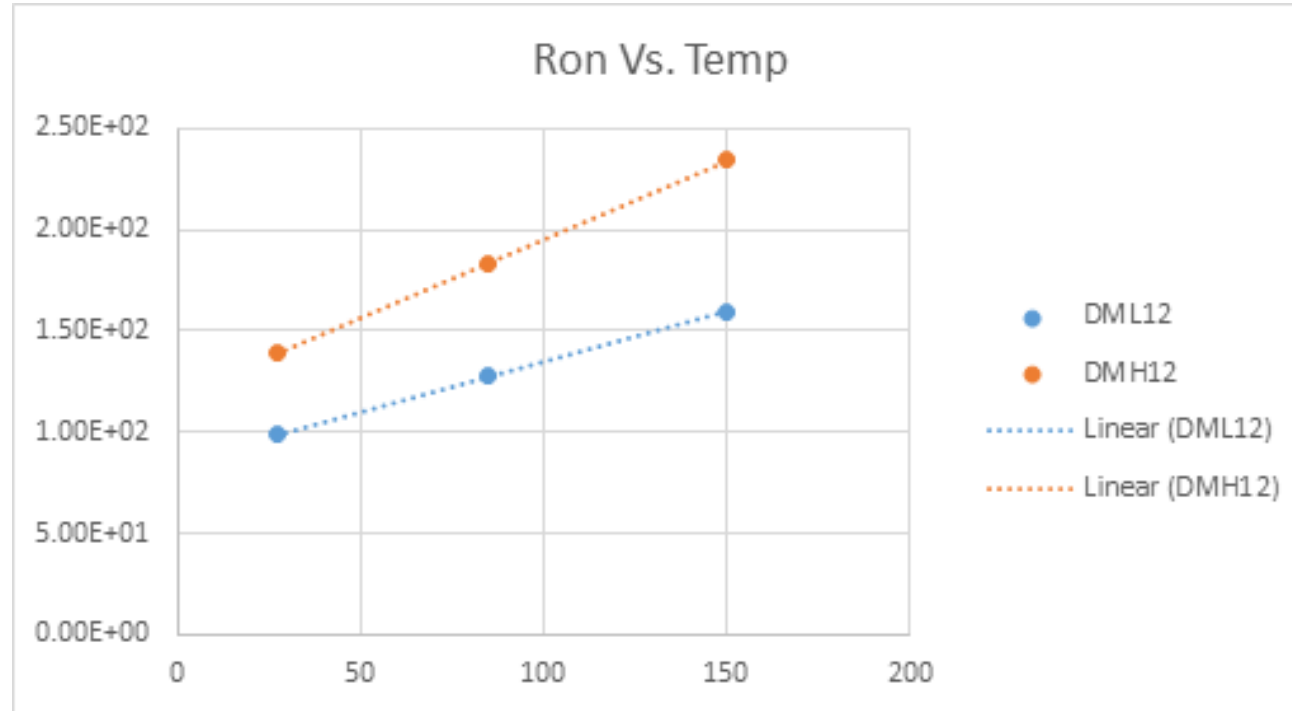
Operating supply current		no PWM, no load, nSLEEP_HB=5V, nSLEEP_LDO=0		900	1200	μA
		50-kHz PWM, no load, nSLEEP_HB=5V, nSLEEP_LDO=0		1.2	1.5	mA

Output rise time		RL=20 Ω	30		200	ns
Output fall time		RL=20 Ω	30		200	ns

Let's assume you are driving a load with 5V, 2A output current with a PWM frequency of:

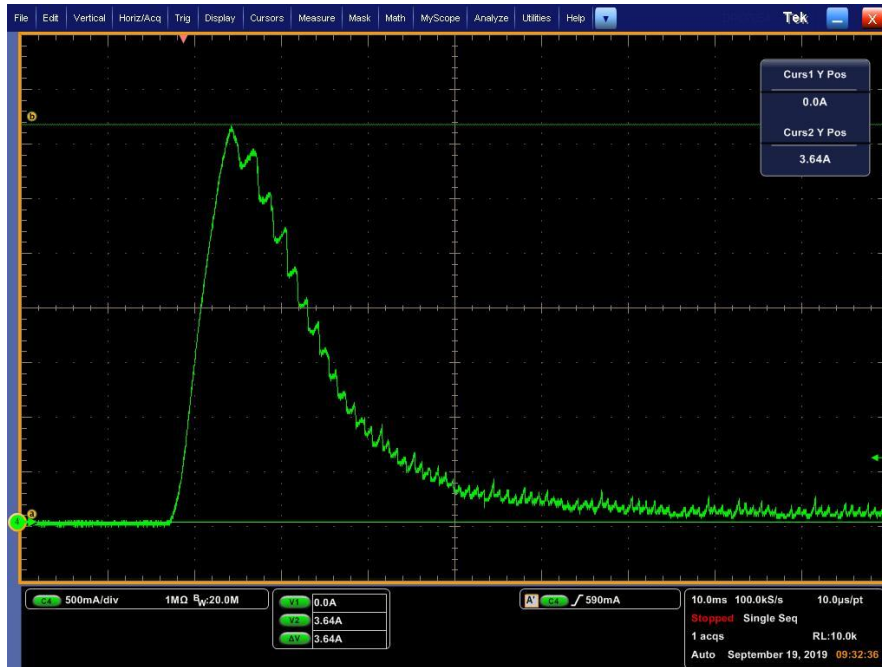
- Using the $R_{DS(ON)}$, we will dissipate $(5A)^2 \times 0.1\Omega = 0.25W$ in the high side, and $(5A)^2 \times 0.1\Omega = 0.25W$ in the low side
- Static power will be $5V \times 1.2mA = 0.006W$
- Switching loss is approximately $(1/2 \times 100ns \times 50kHz \times 5V \times 2A) + (1/2 \times 100ns \times 50kHz \times 5V \times 2A) = 0.05W$
- Total power is then 0.56W

A Problem: $R_{DS(ON)}$ vs. Temperature



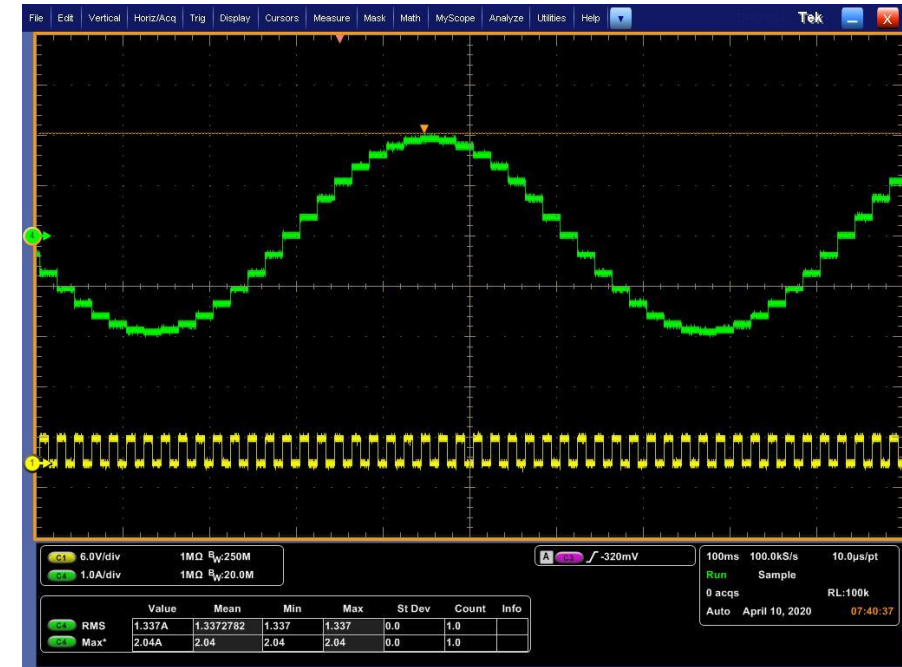
Peak vs. Average and RMS Load Current

DC Motor Start-Up Current



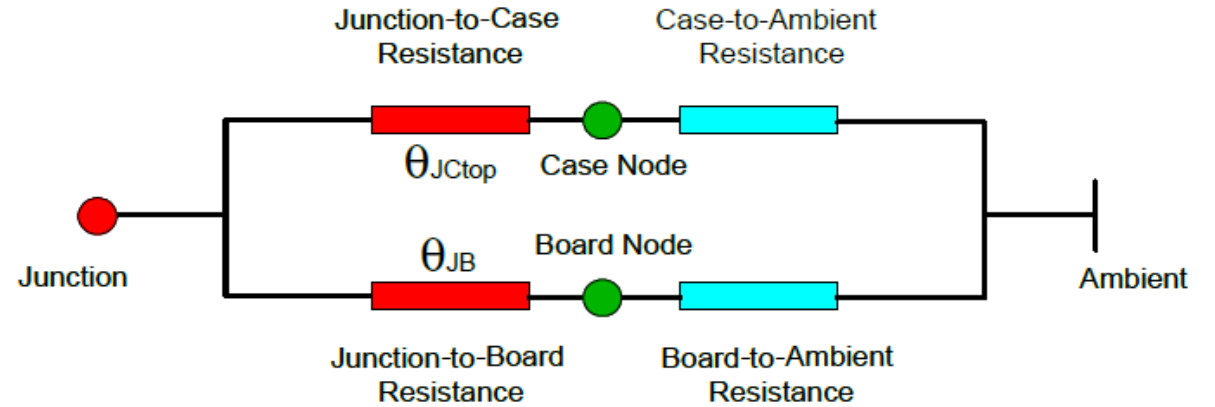
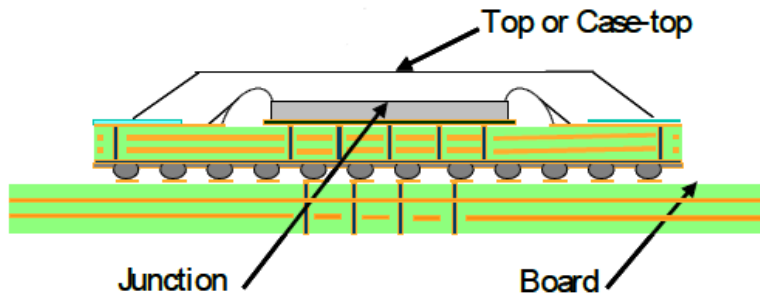
3.6A Peak for ~20ms

Stepper Motor RMS Current



2A peak \approx 1.4A RMS

Thermal Resistance & Models



Simple Estimation:
Die temperature = ambient temp + (P x Θ_{JA})

Temperature Rise Example

Using the MP6550 IC as an example:

Thermal Resistance ⁽⁴⁾ θ_{JA} θ_{JC}
 QFN-12 (2mm×2mm)..... 80 16..... °C/W

Continuous Power Dissipation ($T_A = +25^\circ\text{C}$) ⁽²⁾
1.56W

Thermal Shutdown Threshold ^(b)	T_{TSD}			160		°C
Thermal Shutdown Hysteresis ^(b)				25		°C

Total power dissipation is 560mW:

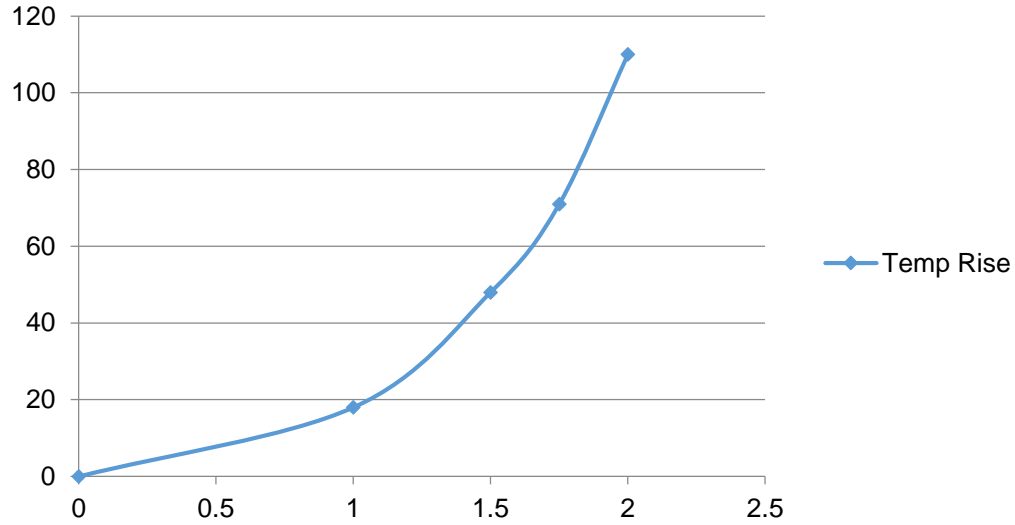
- Temperature rise is $P \times \Theta_{JA}$, so $0.56 \times 80 = 44.8^\circ\text{C}$
- Junction temperature is $T_A + T_R$.
 If we assume room temperature of 25°C , then the junction is at $25 + 44.8 = 69.8^\circ\text{C}$.

If the ambient is 70°C , then the junction temperature will be 114.8°C .

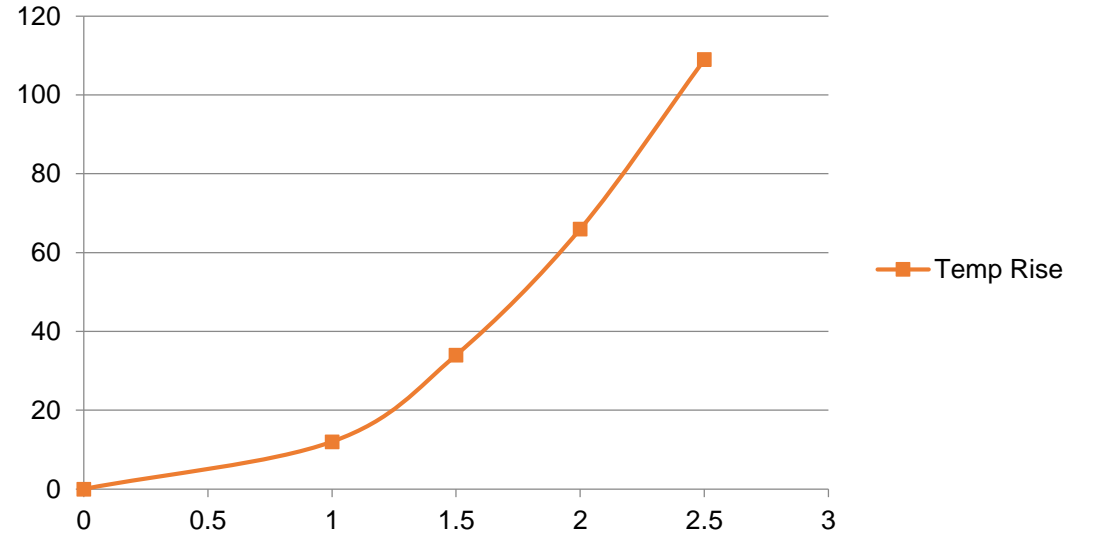
Temperature Rise vs. Output Current

Bigger Package = Better Thermals

Temp Rise MP6600 QFN



Temp Rise MP6500 TSSOP



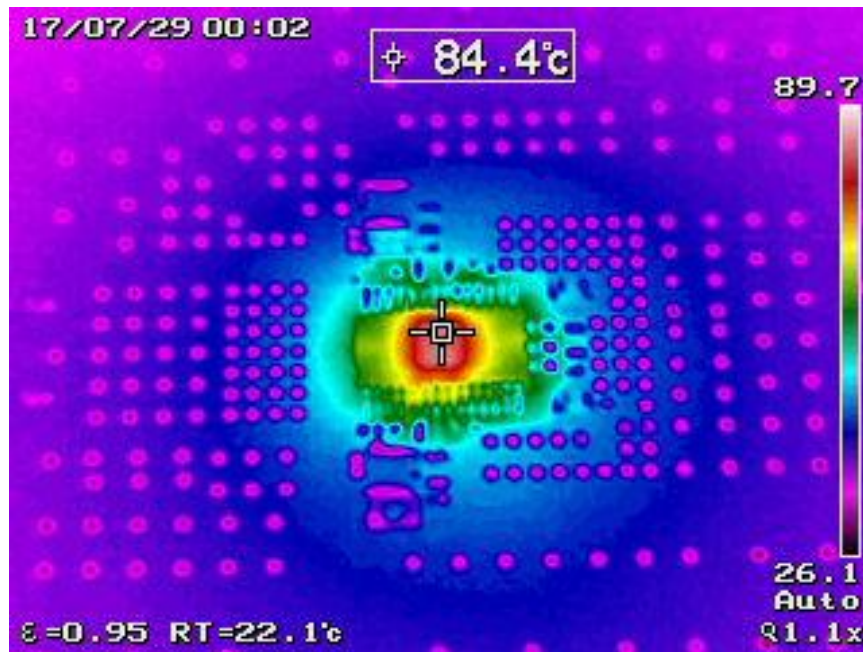
PCB Design for Power Dissipation

Table 7 — JESD51-7 High Thermal Conductivity Leaded SMT Test Board Parameters [8]

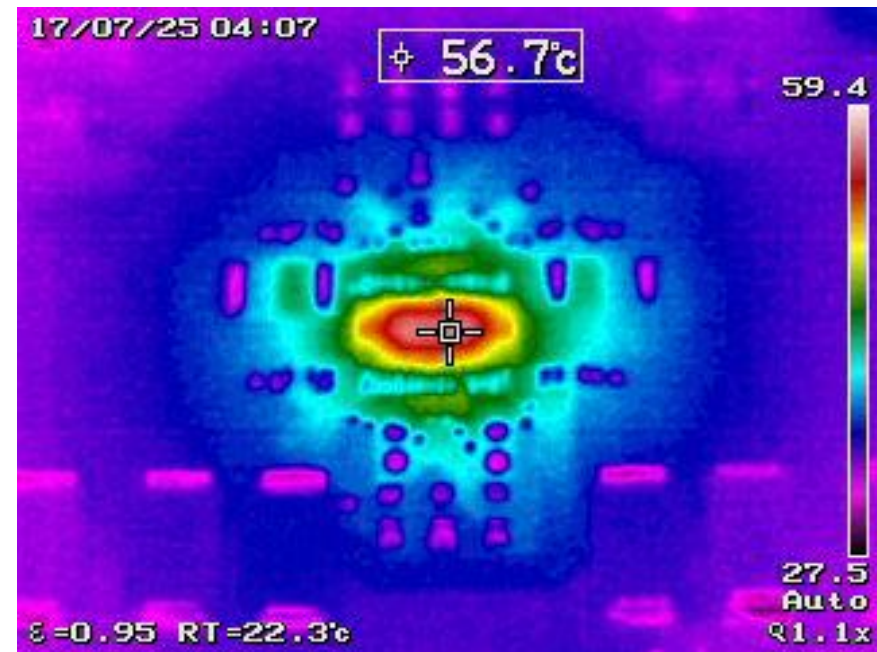
Dimension	Specification	User
Board Finish Thickness	1.60 mm \pm 10%	
Board Dimension (pkg length < 27 mm)	76.2 mm x 114.3 mm	
Board Dimension (27 mm \leq pkg length \leq 48 mm)	101.6 mm x 114.3 mm	
Board material	FR-4	
Trace Copper Thickness	0.070 mm \pm 20%	
Trace Width, Finished	0.25 mm \pm 10% for \geq 0.50 mm pin pitch Lead width for < 0.50 mm pin pitch	
Trace Coverage Area (Total)		
Power/Ground Thickness	35 μ m (1oz) copper +0/-20%	

Effect of Layer Count & Planes

MP6500 Driving 2A Peak Stepper Motor

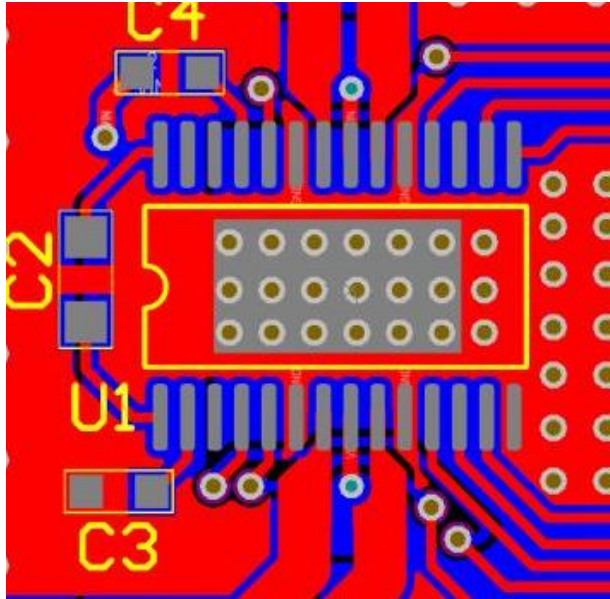
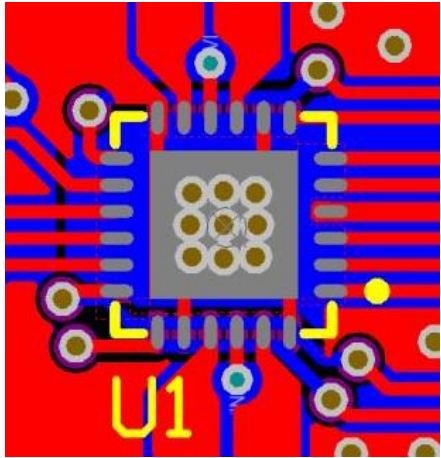
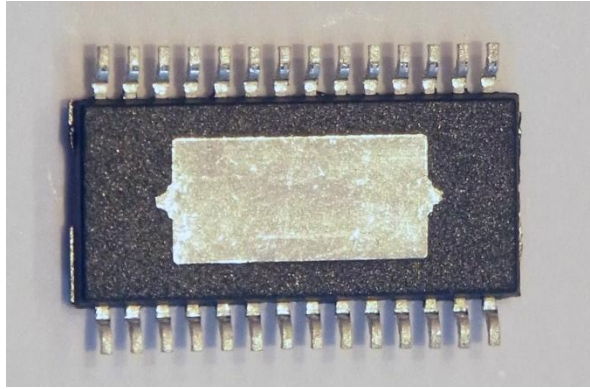
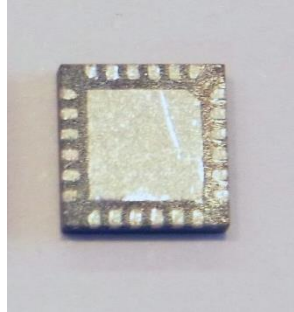


2 Layers

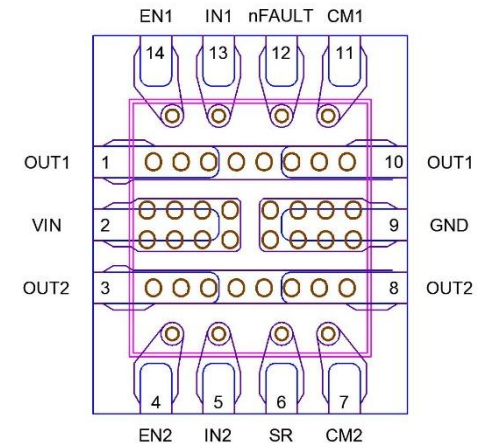
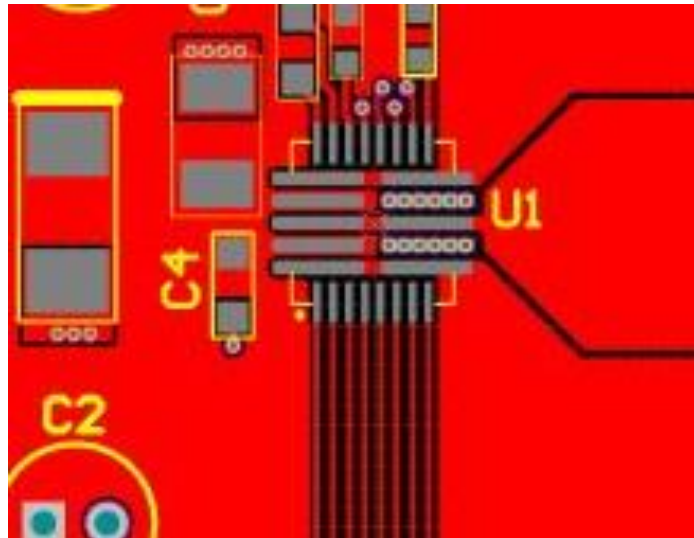
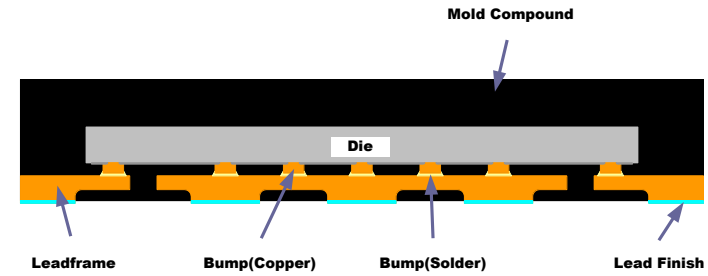
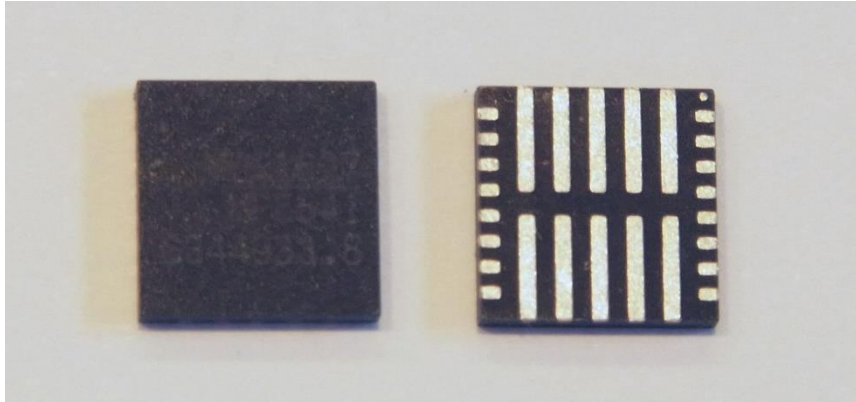


4 Layers (2 Planes)

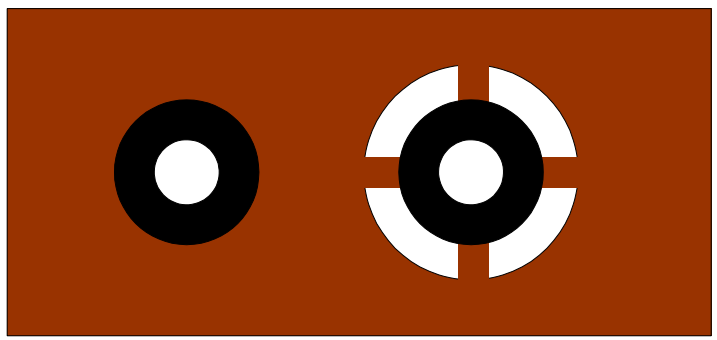
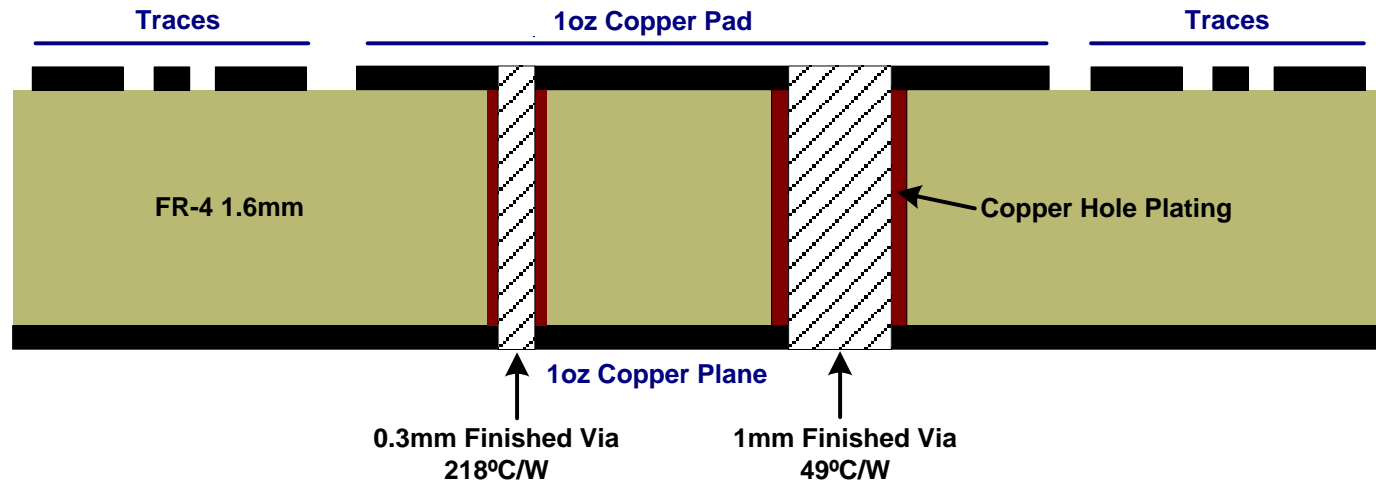
Exposed Pads on TSSOP & QFN



Flip-Chip QFN and LGA Packages



Thermal Vias

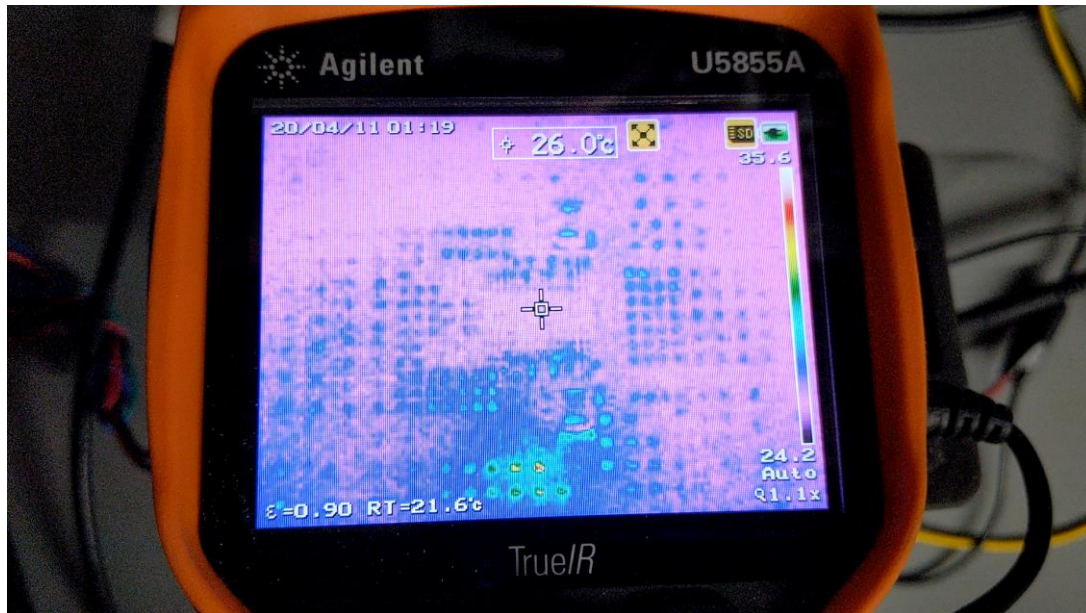


Solid Connection
YES!

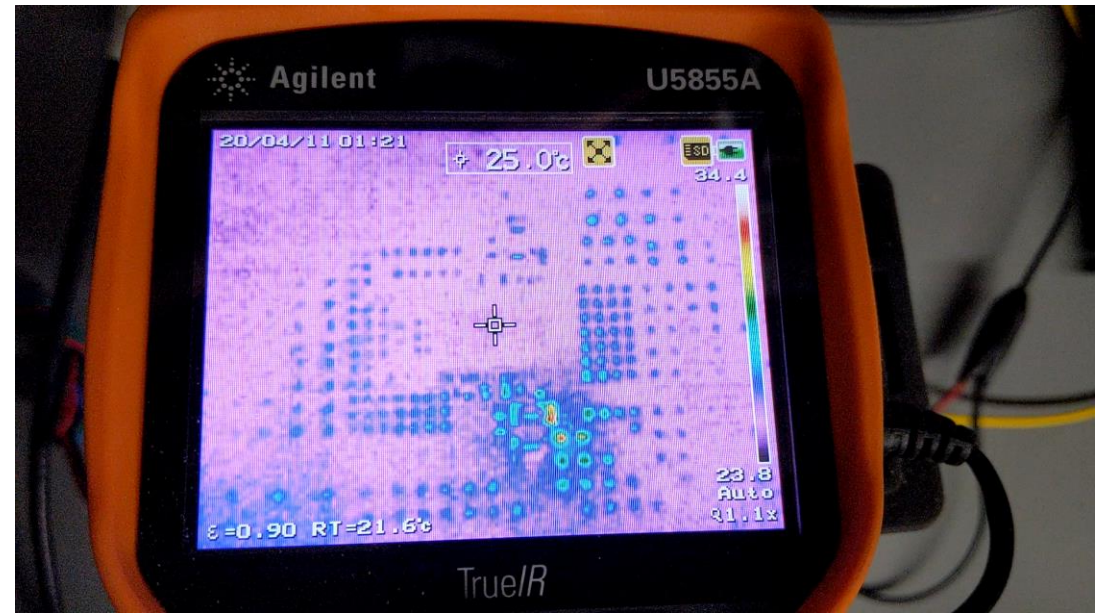
Thermal Relief
NO!

What Happens if the Exposed Pad isn't Soldered?

MP6500 Driving 2A Peak Stepper Motor 4-Layer PCB



Exposed Pad Soldered



Exposed Pad Not Soldered

Summary

- Calculate the power dissipated in your motor driver IC
 - Or work backwards and calculate maximum current from thermal conditions
- Minimize thermal resistance
 - Bigger is always better
 - Multi-layer boards work best
- Use thermal vias to spread heat
- ALWAYS solder the exposed pad

Q&A

Please submit questions through the “Q&A” menu option in the Zoom app

This webinar and others will be available for on-demand streaming at:

MonolithicPower.com/webinars